

# Introduction to Medical Imaging

## Ultrasound Imaging

Klaus Mueller

Computer Science Department

Stony Brook University

## Overview

### Advantages

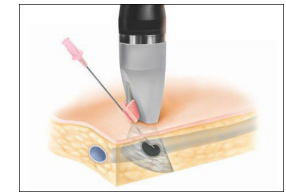
- non-invasive
- inexpensive
- portable
- excellent temporal resolution

### Disadvantages

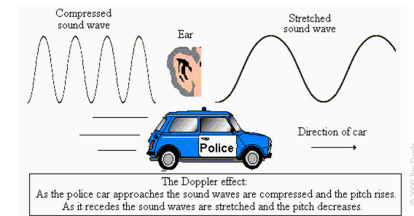
- noisy
- low spatial resolution

### Samples of clinical applications

- echo ultrasound
  - cardiac
  - fetal monitoring
- Doppler ultrasound
  - blood flow
- ultrasound CT
  - mammography



US guided biopsy



Doppler effect

## History

### Milestone applications:

- publication of *The Theory of Sound* (Lord Rayleigh, 1877)
- discovery of piezo-electric effect (Pierre Curie, 1880)
  - enabled generation and detection of ultrasonic waves
- first practical use in World War One for detecting submarines
- followed by
  - non-destructive testing of metals (airplane wings, bridges)
  - seismology
- first clinical use for locating brain tumors (Karl Dussik, Friederich Dussik, 1942)
- the first greyscale images were produced in 1950
  - in real time by Siemens device in 1965
- electronic beam-steering using phased-array technology in 1968
- popular technique since mid-70s
- substantial enhancements since mid-1990



Pierre Curie  
1859 - 1906

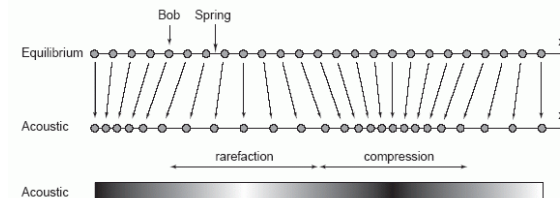


Karl Theodore Dussik

## Ultrasonic Waves

### US waves are longitudinal compression waves

- particles never move far
- transducer emits a sound pulse which compresses the material
- elasticity limits compression and extends it into a *rarefaction*
- rarefaction returns to a compression
- this continues until damping gradually ends this oscillation

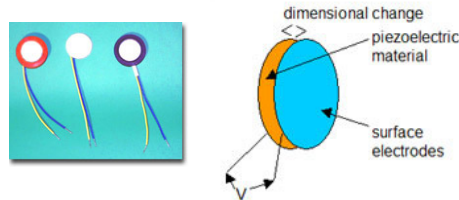


- ultrasound waves in medicine > 2.5 MHz
- humans can hear between 20 Hz and 20 kHz (animals more)

## Generation of Ultrasonic Waves

Via piezoelectric crystal

- deforms on application of electric field → generates a pressure wave
- induces an electric field upon deformation ← detects a pressure wave
- such a device is called *transducer*



## Wave Propagation

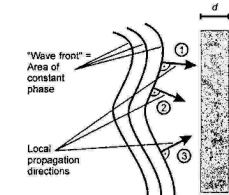
Two equations

• wave equation: 
$$\nabla^2 \Delta p = \frac{1}{c_0} \frac{\partial^2 \Delta p}{\partial t^2} \quad c_0 = \sqrt{\frac{1}{\rho_0 \beta_{s0}}}$$

$\Delta p$ : acoustic pressure,  $\rho_0$ : acoustic density,  $\beta_{s0}$ : adiabatic compressibility

• Eikonal equation:

$$\frac{\partial^2 t}{\partial x^2} + \frac{\partial^2 t}{\partial y^2} + \frac{\partial^2 t}{\partial z^2} = \frac{1}{F^2(x, y, z)}$$



$1/F$ : "slowness vector", inversely related to acoustic velocity  $v$

- models a surface of constant phase called the *wave front*
- sound rays propagate normal to the wave fronts and define the direction of energy propagation.

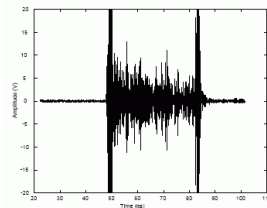
## Effects in Homogeneous Media

Attenuation

- models the loss of energy in tissue

$$H(f, z) = e^{-a_0 f^n z}$$

- $f$ : frequency, typically  $n=1$ ,  $z$ : depth,  $a_0$ : attenuation coefficient of medium,



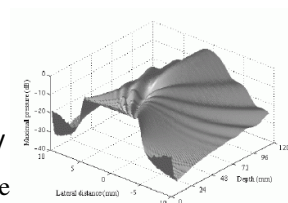
Non-linearity

- wave equation was derived assuming that  $\Delta p$  was only a tiny disturbance of the static pressure
- however, with increasing acoustic pressure, the wave changes shape and the assumption is violated

Diffraction

- complex interference pattern greatest close to the source
- further away point sources add constructively

simulation with a circular planar source



## Effects in Non-Homogeneous Media (1)

Reflection and refraction

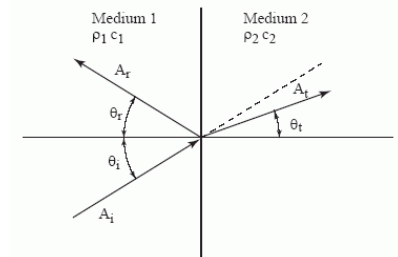
- at a locally planar interface the wave's frequency will not change, only its speed and angle

$$\frac{\sin \theta_i}{c_1} = \frac{\sin \theta_r}{c_1} = \frac{\sin \theta_t}{c_2}$$

- for  $c_2 > c_1$  and  $\theta_i > \sin^{-1}(c_1/c_2)$  the reflected wave will not be in phase when

$$\cos \theta_i = \sqrt{1 - \left(\frac{c_2}{c_1} \sin \theta_i\right)^2}$$

is complex



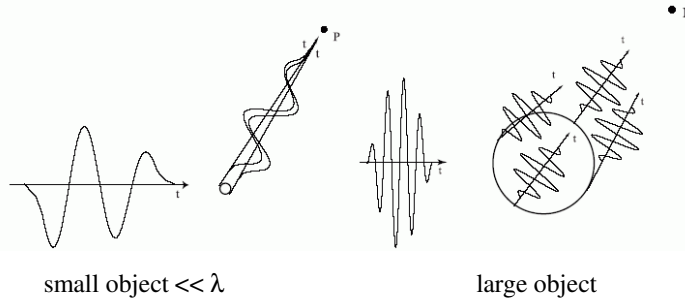
- the amplitude changes as well:  $T+R=1$ ,  $Z=\rho v$

$$T = \frac{A_t}{A_i} = \frac{2Z_1 \cos \theta_i}{Z_2 \cos \theta_i + Z_1 \cos \theta_i} \quad R = \frac{A_r}{A_i} = \frac{Z_2 \cos \theta_i - Z_1 \cos \theta_i}{Z_2 \cos \theta_i + Z_1 \cos \theta_i}$$

## Effects in Non-Homogeneous Media (2)

### Scattering

- if the size of the scattering object is  $\ll \lambda$  then get constructive interference at a far-enough receiver P
- if not, then need to model scattering as many point scatterers for a complex interference pattern



## Data Acquisition: A-Mode

### 'A' for Amplitude

Simplest mode (no longer in use), basically:

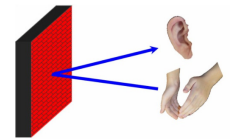
- clap hands and listen for echo:

$$\text{distance} = \frac{\text{time expired} \cdot \text{speed of sound}}{2}$$

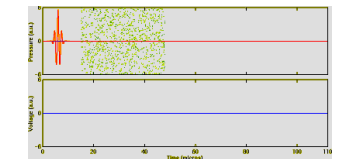
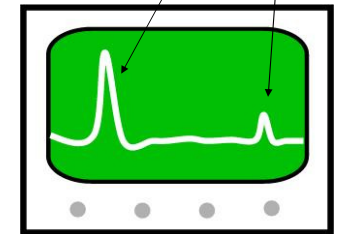
- time and amplitude are almost equivalent since sound velocity is about constant in tissue

Problem: don't know where sound bounced off from

- direction unclear
- shape of object unclear
- just get a single line



pulse sent out →      ← echo received



## Data Acquisition: M-Mode

### 'M' for Motion

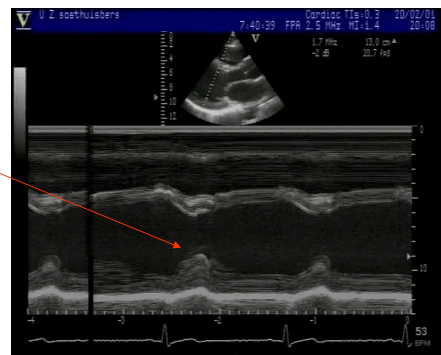
Repeated A-mode measurement

Very high sampling frequency: up to 1000 pulses per second

- useful in assessing rates and motion
- still used extensively in cardiac and fetal cardiac imaging

motion of heart wall during **contraction**

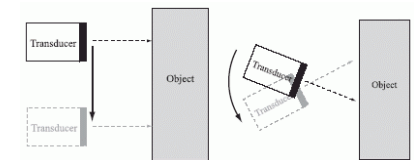
blood  
heart muscle  
pericardium



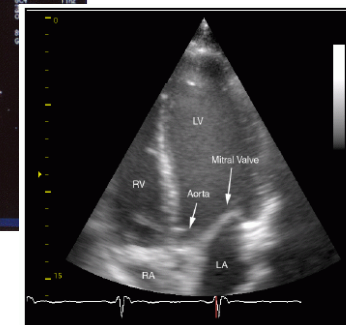
## Data Acquisition: B-Mode

### 'B' for Brightness

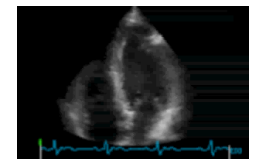
An image is obtained by translating or tilting the transducer



fetus



normal heart



continuous

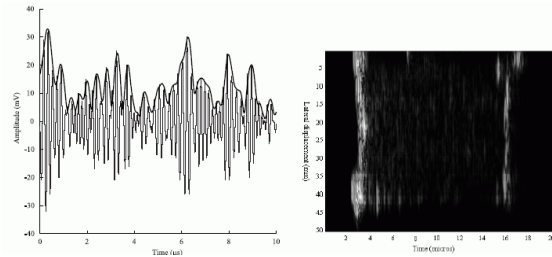
## Image Reconstruction (1)

### Filtering

- remove high-frequency noise

### Envelope correction

- removes the high frequencies of the RF signal



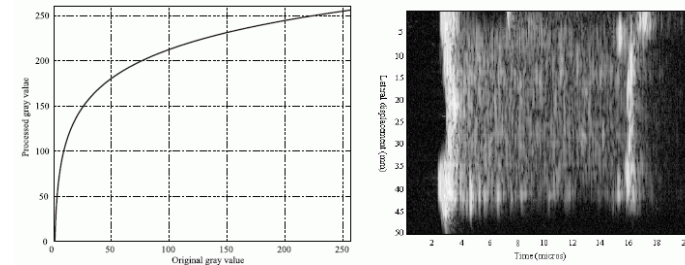
### Attenuation correction

- correct for pulse attenuation at increasing depth
- use exponential decay model

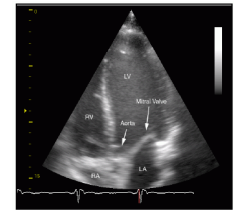
## Image Reconstruction (2)

### Log compression

- brings out the low-amplitude speckle noise



- speckle pattern can be used to distinguish different tissue



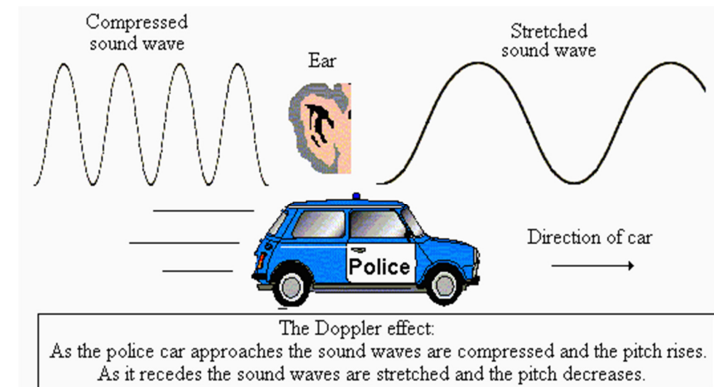
## Acquisition and Reconstruction Time

Typically each line in an image corresponds to 20 cm

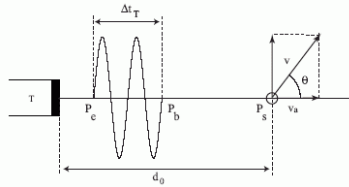
- velocity of sound is 1540 m/s  
→ time for line acquisition is 267  $\mu$ s
- an image with 120 lines requires then about 32 ms  
→ can acquire images at about 30 Hz (frames/s)
- clinical scanners acquire multiple lines simultaneously and achieve 70-80 Hz



## Doppler Effect: Introduction



## Doppler Effect: Fundamentals (1)



Assume an acoustic source emits a pulse of  $N$  oscillation within time  $\Delta t_T$

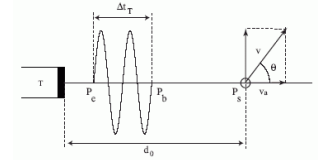
- a point scatterer  $P_s$  travels at axial velocity  $v_a$ :
- the locations of the wave and the scatterer are:  $P_b(t) = ct$   $P_s(t) = d_0 + v_a t$
- the start of the wave meets  $P_s$  at:  

$$P_b(t_{ib}) = P_s(t_{ib}) \rightarrow t_{ib} = \frac{d_0}{c - v_a}$$
- the end of the wave meets  $P_s$  at:

$$P_b(t_{ie}) = P_s(t_{ie}) \rightarrow t_{ie} = \frac{d_0 + c\Delta t_T}{c - v_a} = t_{ib} + \frac{c}{c - v_a} \Delta t_T$$

- the start of the wave meets the transducer at  $t_{rb} = 2t_{ib}$
- the end of the wave meets the transducer at  $t_{re} = 2t_{ie} - \Delta t_T$

## Doppler Effect: Fundamentals (2)



Received pulse ( $N$  oscillations)

- the duration of the received pulse is  $\Delta t_R = t_{re} - t_{rb} = \left(\frac{2c}{c - v_a} - 1\right) \Delta t_T$
- writing it as frequencies  $f_T = \frac{N}{\Delta t_T}$   $f_R = \frac{N}{\Delta t_R}$
- the Doppler frequency is then  $f_D = f_R - f_T = \frac{-2v_a}{c + v_a} f_T \approx \frac{-2v_a \cos \theta}{c} f_T$
- to hear this frequency, add it to some base frequency  $f_b$
- finally, to make the range smaller,  $f_d$  may have to be scaled

Example:

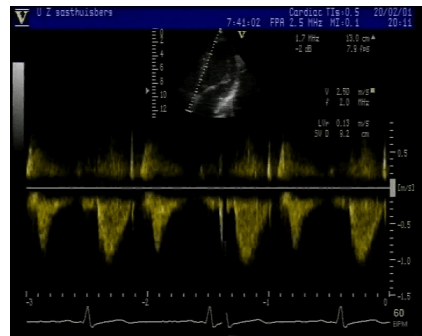
- assume a scatterer moves away at 0.5 m/s, the pulse frequency is 2.5 MHz, and a base frequency of 5 kHz, then the shift is an audible 5 kHz - 1.6 kHz = 3.4 kHz

## Doppler: CW

'CW' for Continuous Wave

Compare frequency of transmitted wave  $f_T$  with frequency of received wave  $f_R$

- the Doppler frequency is then:  $f_D = f_R - f_T = \frac{-2v_a}{c + v_a} f_T \approx \frac{-2|v_a| \cos \theta}{c} f_T$
- Doppler can be made audible, where pitch is analog to velocity



## Doppler: PW (1)

'PW' for Pulsed Wave

Does not make use of the Doppler principle

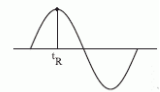
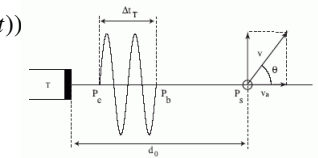
- instead, received signal is assumed to be a scaled, delayed replica of the transmitted one

$$s(t) = A \sin(2\pi f_T(t - \Delta t))$$

$\Delta t$  is the time between transmission and reception of the pulse  
it depends on the distance between transducer and scatterer

- in fact, we only acquire one sample of each of the received pulses, at  $t_R$ :

$$s(t_R) = A \sin(2\pi f_T(t_R - \Delta t))$$



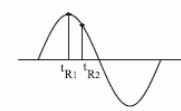
- now, if the scatterer moves away at velocity  $v_a$ , then the distance increases with  $v_a T_{PRF}$  ( $T_{PRF}$ : pulse repetition period)
- this increases the time  $\Delta t$  (or decreases if the scatterer comes closer)



## Doppler: PW (2)

Thus, the sampled sequence  $s_j$  is:

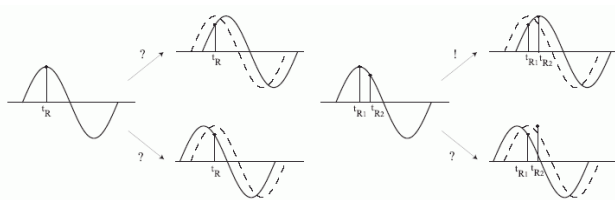
$$s_j = A \sin(-2\pi f_T (j \cdot \frac{2 \cdot v_a T_{PRF}}{c}) + B)$$



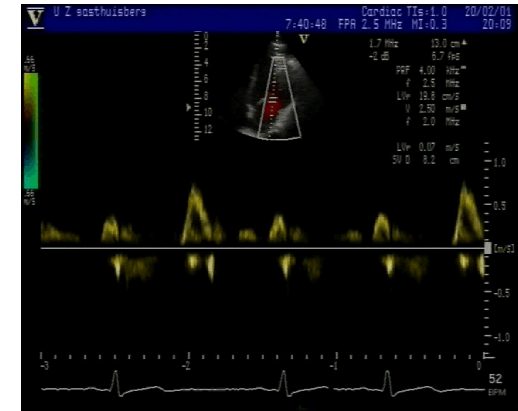
- therefore, the greater  $v_a$ , the higher the frequency of the sampled sinusoid:

$$f_D = -\frac{2v_a}{c} f_T$$

- to get direction information, one must sample more than once per pulse (twice per half oscillation) :



## Doppler: PW (3)

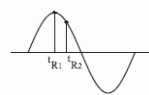


## Color Flow Imaging: Technique

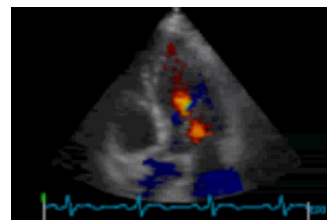
Calculates the phase shift between two subsequently received pulses

$$\Delta\phi = 2\pi f_T (\frac{2 \cdot v_a T_{PRF}}{c})$$

- measure the phase shift by sampling two subsequent pulses at two specific time instances  $t_{R1}$  and  $t_{R2}$

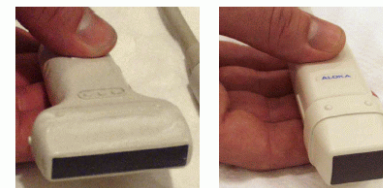


- since this can become noisy, usually the results of 3-7 such samplings (pulses) are averaged
- divide the acquired RF line into segments (range gates) allows velocities to be obtained at a number of depths
- acquiring along a single line gives a M-mode type display
- acquiring along multiple lines enables a B-mode type display



red: moving toward transducer  
blue: moving away from transducer

## Ultrasound Equipment



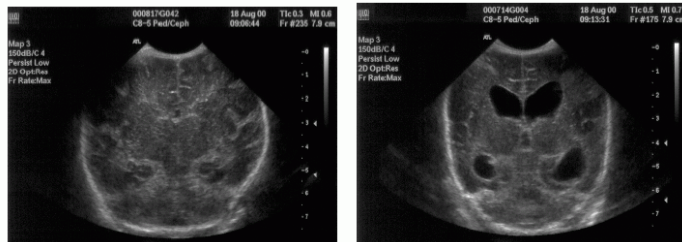
Left: Linear array transducer.

Right: Phased array transducer



commercial echocardiographic scanner

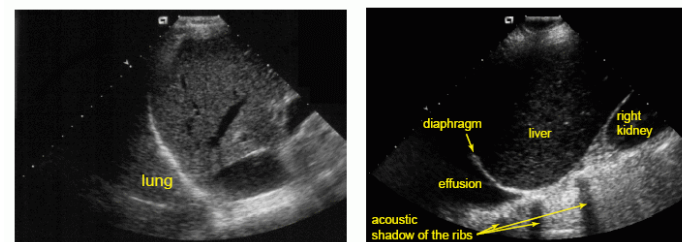
## Ultrasound Applications (1)



Left: Normal cranial ultrasound.

Right: Fluid filled cerebral cavities on both sides as a result of an intraventricular haemorrhage

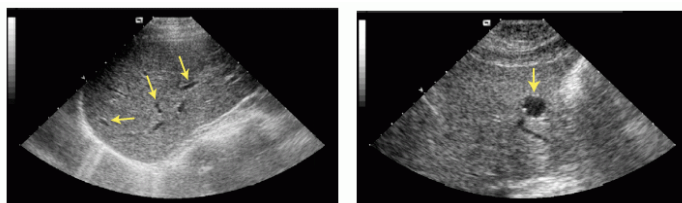
## Ultrasound Applications (2)



Left: normal lung,

Right: pleural effusion

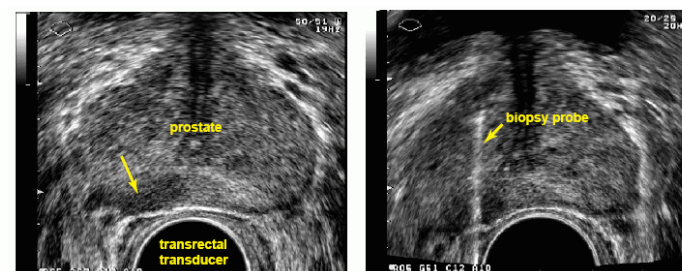
## Ultrasound Applications (3)



Left: normal liver

Right: liver with cyst

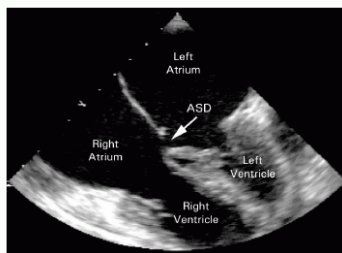
## Ultrasound Applications (4)



Left: prostate showing a hypoechoic lesion suspicious for cancer

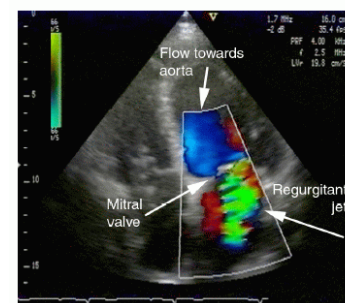
Right: with biopsy needle

## Ultrasound Applications (5)



Atrial septal defect (ASD)

## Ultrasound Applications (6)



Doppler color flow image of a patient with mitral regurgitation in the left atrium. The bright green color corresponds to high velocities in mixed directions, due to very turbulent flow leaking through a small hole in the mitral valve.